

5 **Comparative Influence of Cohesion and Friction Angle on the Stability of**
6 **Dry Slopes: A Parametric Sensitivity Study of Ramche Landslide**

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12
13 **Abstract**

14 The reliability and safety of slope designs largely depend on accurately understanding and measuring
15 the soil properties of slope, because small errors in estimating this parameter can significantly affect
16 stability predictions. This study investigates the sensitivity of slope stability to variations in cohesion
17 (c) and internal friction angle (ϕ) with respect to the Factor of Safety (FoS). The research focuses on
18 the Ramche landslide in Rasuwa District, Nepal, representing a typical Himalayan slope condition.
19 Six disturbed and undisturbed soil samples were collected from different locations along the slope
20 profile during a detailed field investigation. Laboratory testing was conducted to determine key
21 engineering properties, including cohesion, friction angle, and unit weight. Based on field
22 measurements, slope geometry was prepared using AutoCAD and SW DTM software, and a
23 numerical model was developed in Slide2. The soil behavior was simulated using the Mohr–
24 Coulomb failure criterion. Slope stability was evaluated using four limit equilibrium methods:
25 Bishop Simplified method, Janbu Simplified method, Spencer method, and Morgenstern–Price
26 method. Sensitivity analyses, including tornado and spider plots, indicate that ϕ is the most
27 influential parameter, producing significantly greater variation in FoS compared to cohesion. The
28 results consistently show that slope stability is more sensitive to uncertainties in the friction angle,
29 highlighting the importance of accurate shear strength characterization for reliable slope design and
30 risk assessment.

31 **Keywords:** Sensitivity analysis of slope, Slide2 numerical modeling, Cohesion and friction
32 angle, Factor of Safety

35 1. Introduction

36 Landslides represent one of the most persistent and destructive natural hazards affecting
37 mountainous regions worldwide (Osman, 2018). In countries characterized by steep terrain,
38 intense rainfall, and fragile geological formations, slope failures frequently disrupt
39 communities, damage infrastructure, and hinder sustainable development. Nepal, situated in
40 the central Himalaya, exemplifies this vulnerability. The country's dramatic topographic relief
41 from the low-lying Terai plains to the towering peaks of the Mountain region creates sharp
42 elevation gradients within a relatively short north-south distance (Chhetri and Easterling, 2010).
43 Such geomorphological conditions, combined with active tectonics and seasonal monsoon
44 precipitation (Shrestha et al., 2000, Sharma et al., 2020), make slope instability a recurring and
45 critical national concern. In this context, understanding the mechanical behavior of slopes and
46 the parameters that govern their stability is not only an academic pursuit but also a practical
47 necessity for engineering design and disaster risk reduction.

48 To appreciate the complexity of slope failures in Nepal, it is important to define several key
49 concepts. A landslide is the downslope movement of soil, rock, and debris under the influence
50 of gravity, often triggered by external factors such as rainfall, earthquakes, or human activity
51 (Skilodimou et al., 2018, Ahmed, 2021, Highland and Bobrowsky, 2008). The stability of a
52 slope is commonly evaluated using the FoS, defined as the ratio of resisting forces to driving
53 forces. When the FoS is greater than one, the slope is considered stable; when it approaches or
54 falls below one, failure becomes likely. The shear strength of soil, a fundamental property
55 governing slope stability, is primarily described by two parameters derived from the Mohr
56 Coulomb failure criterion: cohesion (c), representing the bonding between particles, and
57 friction angle (ϕ), representing the internal resistance due to particle interlocking and friction.
58 Variations in these parameters whether due to changes in moisture content, weathering, or
59 stress conditions can significantly influence the FoS and, consequently, slope performance
60 (Iverson, 2000, Medina et al., 2021, Malla and Dahal, 2021).

61 In Nepal, more than seventy-five percent of the annual rainfall occurs during the monsoon
62 season, typically from June to September (Shrestha et al., 2000, Sharma et al., 2020). This
63 intense and prolonged precipitation increases soil moisture, raises groundwater levels, and
64 reduces effective stress within slopes (Findell and Eltahir, 1997). As pore water pressure rises,
65 the apparent cohesion and effective friction angle may decrease, thereby reducing shear
66 strength (Iverson, 2000, Medina et al., 2021, Malla and Dahal, 2021, Baral et al., 2025, Baral
67 and Tiwari, 2025). Numerous studies have identified monsoon rainfall as the primary triggering

68 mechanism for slope failures in the Himalayan region (Dahal, 2012, Gnyawali et al., 2023,
69 Kincey et al., 2024). Furthermore, rapid infrastructure expansion such as road construction,
70 hydropower development, and urban growth has altered natural slope geometries and drainage
71 conditions, exacerbating instability in many areas (McAdoo et al., 2018, Paudyal et al., 2023).
72 Although extensive research has been conducted on landslide occurrence, mapping, and rainfall
73 thresholds in Nepal (Dahal and Hasegawa, 2008, Basnet and Acharya, 2019), a critical gap
74 remains in site-specific geotechnical investigations that quantitatively evaluate how variations
75 in shear strength parameters influence slope stability. Many existing studies provide regional-
76 scale hazard assessments or focus on identifying triggering factors, yet fewer studies
77 systematically examine the sensitivity of the FoS to changes in cohesion and friction angle at
78 the local scale. In practice, soil parameters are inherently uncertain due to spatial variability,
79 limited sampling, and laboratory testing constraints (Stark et al., 2008). Designers often rely
80 on representative or conservative values without fully understanding how small deviations in
81 these parameters may affect stability outcomes. Neglecting to analyze parameter sensitivity
82 may produce either excessively conservative designs that drive up costs or overly optimistic
83 assumptions that could endanger safety.

84 Previous analytical approaches to slope stability have predominantly employed the Limit
85 Equilibrium Method (LEM), including Bishop's simplified method, Fellenius' method, and
86 Janbu's method (Li et al., 2019, Zhu et al., 2003). These techniques divide the slope into slices
87 and satisfy force and moment equilibrium to compute the FoS (Zolkepli et al., 2019). LEM
88 remains widely used due to its conceptual simplicity and computational efficiency (Aryal,
89 2006, Liu et al., 2015). More recently, numerical methods such as the Finite Element Method
90 (FEM) have gained prominence relationships (Matthews et al., 2014, Hammouri et al., 2008,
91 Salih, 2021, Griffiths and Lane, 1999). FEM-based approaches, particularly those employing
92 the Shear Strength Reduction (SSR) technique, enable simulation of stress-strain behavior and
93 progressive failure mechanisms (Ramadhani and Ihzan, 2023, VandenBerge and McGuire,
94 2019). Despite these advancements, many applications in Nepal have focused on obtaining a
95 single FoS value under assumed parameter sets, rather than conducting comprehensive
96 sensitivity analyses that explore the relative influence of cohesion and friction angle on slope
97 stability.

98 The rationale for this study arises from the recognition that cohesion and friction angle are not
99 fixed constants but variable properties influenced by geological conditions, weathering,
100 saturation, and sampling uncertainty (Abramson et al., 2001). A rigorous sensitivity analysis
101 provides insight into which parameter exerts the greatest control on the FoS and how variations

102 within realistic ranges affect slope safety. Such understanding is essential for prioritizing field
103 investigations, optimizing laboratory testing programs, and improving the reliability of
104 geotechnical designs. Moreover, in data-scarce mountainous environments, identifying the
105 most influential parameters can guide resource allocation and risk mitigation strategies.

106 Accordingly, the primary objective of this paper is to investigate the sensitivity of slope
107 stability to variations in cohesion and friction angle with respect to the FoS. The study focuses
108 on a representative Himalayan slope in Nepal, where six soil samples were collected from
109 different locations along the Ramche slope profile. The soil mass is modeled as a single
110 homogeneous layer to isolate the effects of shear strength parameters. The FoS is computed
111 using Bishop Simplified method, Janbu Simplified method, Spencer method, and
112 Morgenstern–Price method implemented in Slide 2D software. External influences such as
113 building loads and seismic forces are not considered in order to concentrate specifically on the
114 intrinsic material parameters. By systematically varying cohesion and friction angle within
115 plausible ranges, the research quantifies their relative impact on FoS and identifies the
116 parameter to which the slope is most sensitive.

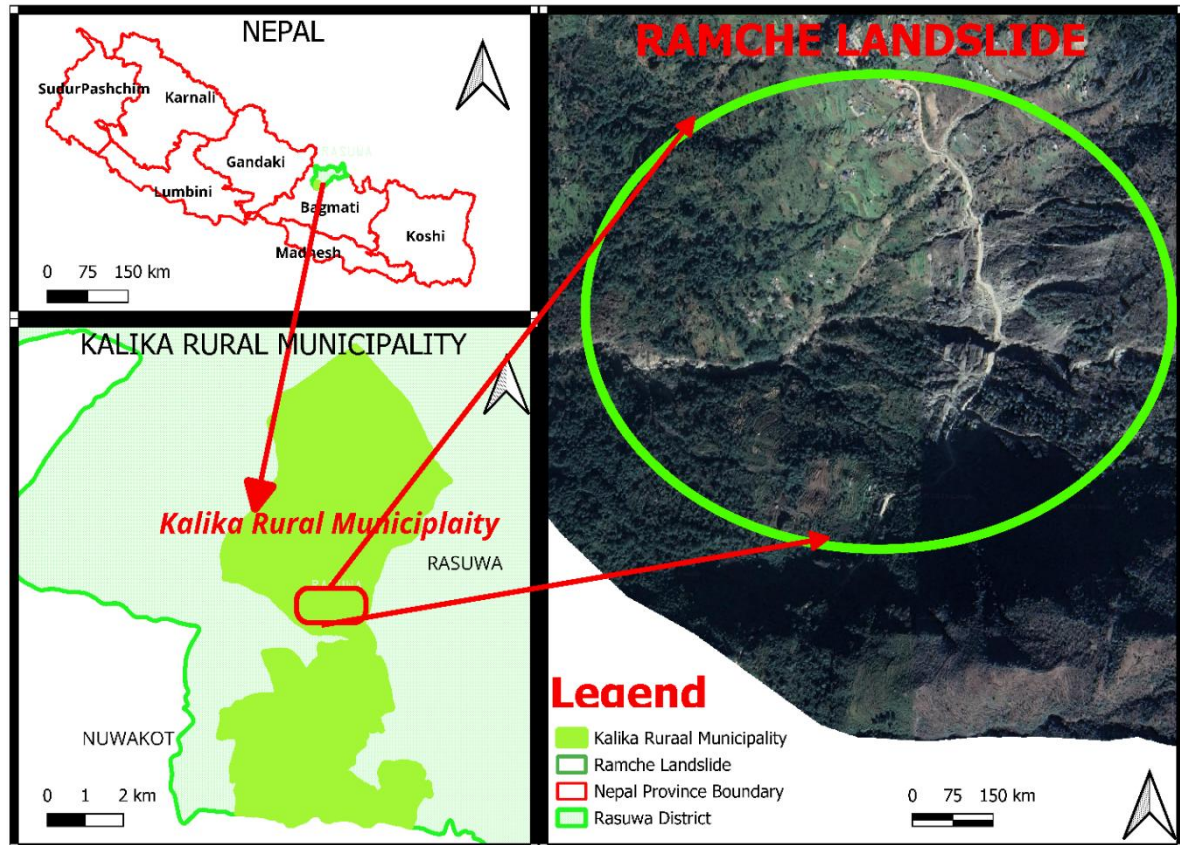
117 **2. Materials and Methods**

118 **2.1. Study area**

119 The study area is located at the Ramche landslide in Rasuwa District, Nepal (Figure 1), along
120 the 36-km section of the Trishuli–Dhunchhe road at 28.026072 N, 85.223361 E above the Trisuli
121 River. Geologically, the site lies within the Kuncha Formation of the Lower Nawakot Group
122 in central Nepal (Jharendra et al., 2018). These rocks are highly weathered and fractured,
123 making the slope weak and vulnerable to failure. The Ramche landslide is classified as a debris
124 flow type movement (Jharendra et al., 2018). It extends for more than 3 km downslope and
125 regularly damages the road section. According to local residents, the landslide was first
126 activated in 1983 and reactivated on 14 August 2003, causing significant loss of life and
127 property (Ghimire et al., 2007). Since then, it has remained active, especially during the
128 monsoon season.

129 High rainfall increases pore water pressure in the slope materials, reducing soil strength and
130 triggering debris movement over the bedrock. In addition, heavy traffic vibrations along the
131 highway further destabilize the slope (Ghimire et al., 2007, Jharendra et al., 2018). Human
132 activities such as haphazard road cutting, unplanned settlements, and unscientific agricultural
133 practices have increased the size and intensity of the landslide. The absence of proper
134 geotechnical mitigation measures has further increased the vulnerability of the area. The

135 surrounding area is densely populated and widely used for cultivation, placing local
 136 communities at high risk. The settlement near the landslide remains in serious danger due to
 137 the continued activity of the slope and the potential for further expansion during intense rainfall
 138 events.

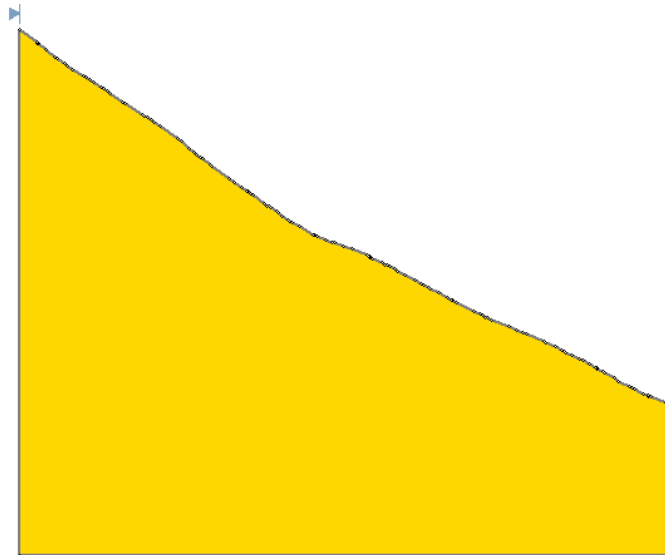


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140 **Figure 1:** Study area map of Ramche Landslide, Rasuwa, Bagmati Province, Nepal

141 The detailed site visit was conducted to collect necessary field information. During the visit,
 142 topographic data, available reports, and soil samples were gathered. Both disturbed and
 143 undisturbed soil samples were collected from six different locations along the slope. These
 144 samples were tested in the laboratory to determine the required engineering properties,
 145 particularly cohesion (c), internal friction angle (ϕ), and unit weight.

146 After obtaining the laboratory results, a numerical model of the slope was developed using
 147 AutoCAD, SW DTM - Software and Slide2. The slope geometry was first defined based on
 148 field measurements in AutoCAD with the help of SW DTM - Software. Then only the model
 149 is prepared in Slide2 (Figure 2). After that, material properties obtained from laboratory testing
 150 were assigned to the model. The soil behavior was simulated using the Mohr–Coulomb failure
 151 criterion, which relates shear strength to cohesion and friction angle.



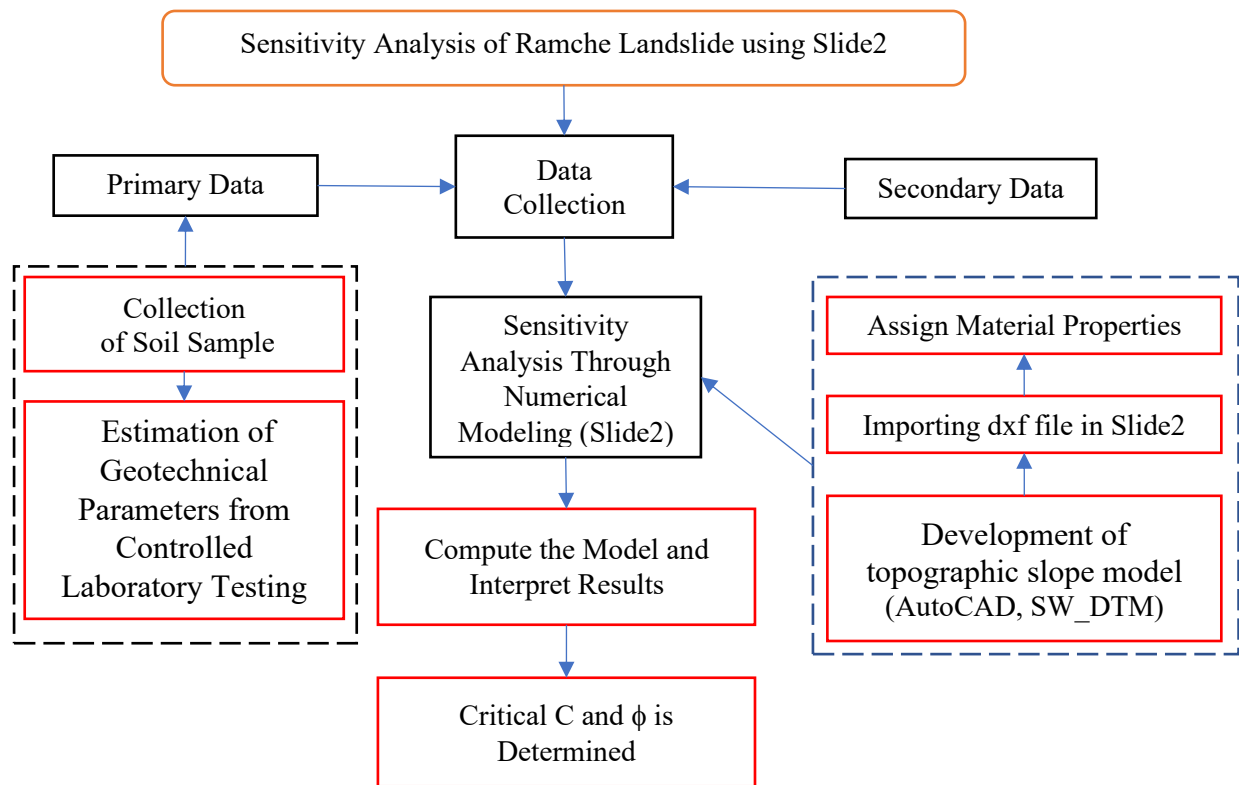
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153 **Figure 2:** Model for Ramche Slope with material assignment (Slide2 model)

154 To ensure uniformity and reliability in the analysis, identical slope geometry was maintained
155 for all simulation cases. Consequently, any observed variation in the FoS can be attributed
156 solely to changes in the shear strength parameters, eliminating the influence of other modeling
157 factors.

158 Slope stability was evaluated using four different limit equilibrium methods: The Bishop
159 Simplified method, Janbu Simplified method, Spencer method, and Morgenstern–Price
160 method. These methods were adopted to evaluate how variations in the assumptions regarding
161 inter-slice force interactions affect the computed FoS. All analyses were performed under dry
162 conditions. Groundwater effects, pore water pressure, surcharge loads, and seismic forces were
163 not included. The earthquake coefficient was set to zero so that the results reflected only the
164 effect of soil shear strength.

165 Finally, a parametric sensitivity analysis was conducted. Cohesion (c) and friction angle (ϕ)
166 were varied systematically within selected ranges, while all other parameters remained
167 constant. For each variation, the model was reanalyzed using all four methods, and the
168 minimum global FoS was recorded. The relationship between FoS and the shear strength
169 parameters was then established to identify which parameter had greater influence on slope
170 stability and to compare the consistency of results among the different methods. Detail work
171 flow is shown in Figure 3.



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Figure 3: Presents the workflow for the numerical and computational analysis.

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3. Results and Discussion

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The case study focuses on a landslide located along the Trishuli Highway at Ramche in Rasuwa District (28.026072° N, 85.223361° E), situated above the Trishuli River. The fundamental soil parameters required for the development of the numerical model were determined through laboratory testing of collected soil samples. These soil parameters were subsequently used to evaluate the sensitivity analysis of the Ramche slope.

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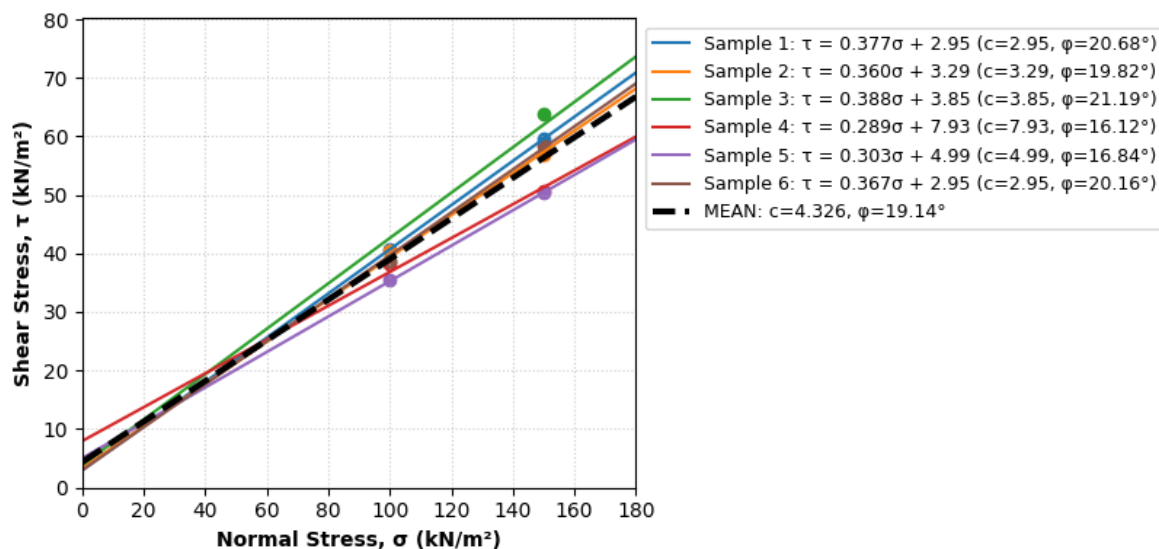
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The results of the direct shear tests demonstrate that the shear strength characteristics of the soil conform to the Mohr–Coulomb failure criterion. This is evidenced by the linear relationship observed between shear stress (y-axis) and normal stress (x-axis), as presented in Figure 4. The shear stress and normal stress relationships derived from the six representative soil samples were used as key input parameters for the sensitivity analysis of the slope. These relationships help to understand how variations in soil strength properties influence the overall stability of the slope and identify which parameters have the most significant impact on potential failure. The dispersion of the plotted data reflects inherent variability in the soil properties, indicating that the slope materials are not perfectly uniform across the site. This natural heterogeneity plays an important role in sensitivity analysis, as even small variations in

190 strength parameters can produce significant changes in the predicted stability condition of the
191 slope.

192 The tested samples show relatively low cohesion values (2.95–7.93 kN/m²) and internal friction
193 angles (16.12°–21.19°), which correspond to limited shear strength. Since cohesion (c) and
194 friction angle (φ) directly govern the shear resistance of soil, minor reductions in these
195 parameters can considerably lower the FoS. This highlights the sensitivity of the slope to
196 variations in shear strength properties and explains its vulnerability to instability under
197 unfavorable conditions. For the sensitivity analysis, the average values of cohesion (4.326
198 kN/m²) and friction angle (19.14°) were adopted as representative baseline parameters. Using
199 the mean values provides a rational and balanced estimate of the overall shear strength of the
200 slope material, minimizing the influence of extreme test results while still reflecting site
201 specific conditions (Duncan et al., 2014, Chowdhury et al., 2023). These average parameters
202 were then systematically varied to evaluate how changes in c and φ affect slope stability,
203 thereby offering a clearer understanding of the slope's response to uncertainty in soil strength
204 characteristics.

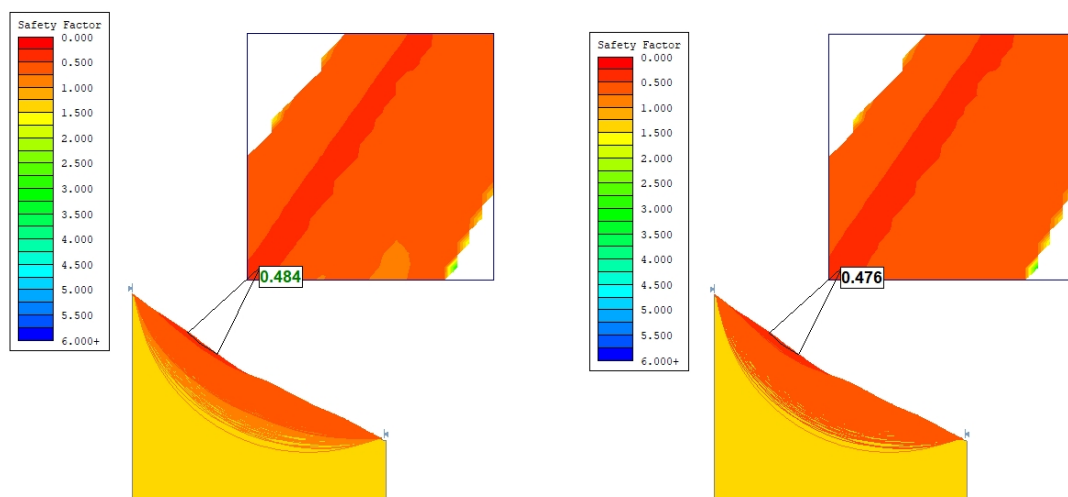


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206 **Figure 4:** Experimental Determination of Shear Strength Parameters Using Direct Shear Test

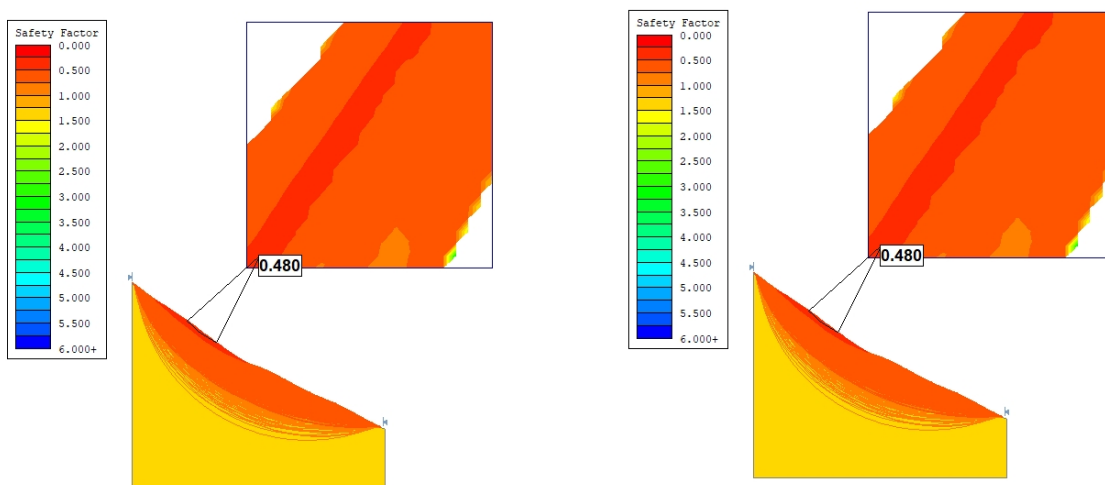
207 The Figure 5 presents the contour distribution of the FoS for the analyzed slope under fully dry
208 and unloaded conditions for the four different methods. The color scale illustrates the variation
209 in stability within the slope mass, where warmer colors such as yellow to red indicate lower
210 FoS values and relatively less stable zones. Most of the slope appears in yellow to light orange
211 shades, suggesting that the FoS is close to 1.0 across a significant portion of the slope.
212 However, the highlighted area identifies a critical zone with a minimum FoS less than one.

213 Because a FoS value less than 1.0 indicates that the available shear strength is insufficient to
 214 resist the driving forces, this result confirms an unstable condition along the identified slip
 215 surface. The contour pattern further reveals a curved failure surface extending from the crest
 216 toward the toe of the slope, which is characteristic of rotational failure in homogeneous soil.
 217 Since groundwater pressure, external surcharge loads, and seismic effects were not considered
 218 in the analysis, the observed instability is attributed solely to inadequate shear strength
 219 parameters, namely cohesion and internal friction angle. These findings demonstrate the high
 220 sensitivity of slope stability to variations in shear strength (Di Matteo et al., 2013, Khan and
 221 Wang, 2021) and indicate that the selected parameter combination is insufficient to maintain
 222 equilibrium under dry conditions.



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 224 (a) Bishop Simplified Method

(b) Janbu Method Simplified



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 226 (c) Spencer Method

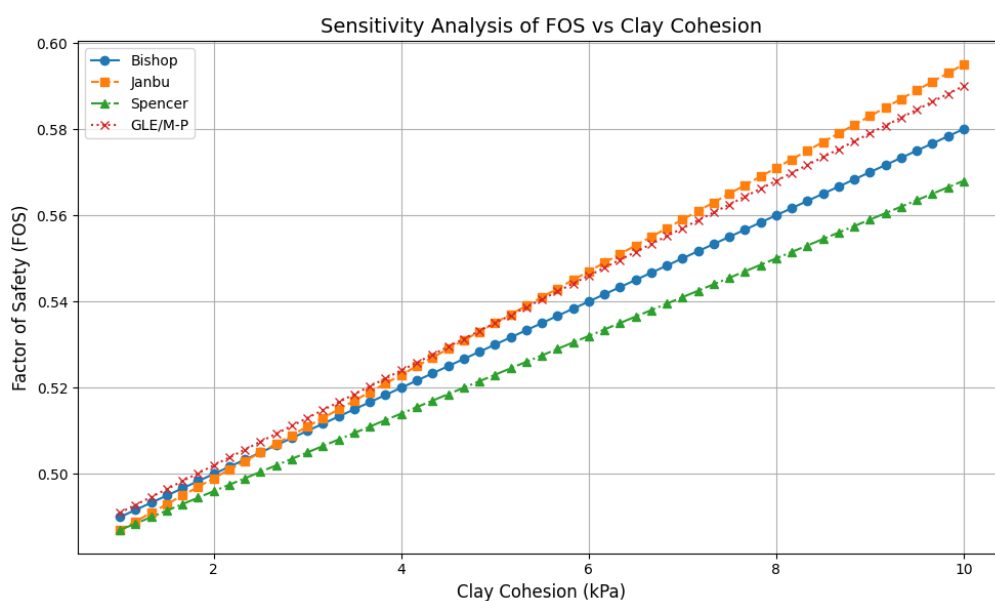
(d) GLE / Morgenstern-Price Method

227 **Figure 5:** Sensitivity analysis of Ramche slope for average base value of Cohesion and
 228 friction angle for obtaining FoS for soil sample

229 The Figure 6 (a and b) illustrates how the FoS varies with changes in clay friction angle and
 230 cohesion using four limit equilibrium methods: Bishop, Janbu, Spencer, and Morgenstern–
 231 Price (GLE). The horizontal axis represents the clay friction angle (Figure 6 a) and cohesion
 232 (Figure 6 b), while the vertical axis shows the corresponding FoS values. A red dashed line
 233 marks the critical stability threshold at $FoS = 1.0$. Across all methods, FoS increases almost
 234 linearly as the friction angle and cohesion increases, clearly demonstrating that slope stability
 235 is strongly controlled by the shear strength contribution from friction angle and cohesion (Khan
 236 and Wang, 2021).

237 At low friction angles, all methods predict FoS values well below 1.0, indicating unstable
 238 conditions. As ϕ increases, FoS gradually improves and crosses the stability threshold at
 239 different points depending on the method. Janbu consistently predicts the highest FoS values,
 240 followed by Morgenstern–Price and Bishop, while Spencer provides slightly lower estimates.
 241 Although there are small differences in magnitude among the methods, the overall trend
 242 remains consistent, confirming that increasing the friction angle significantly enhances slope
 243 stability.

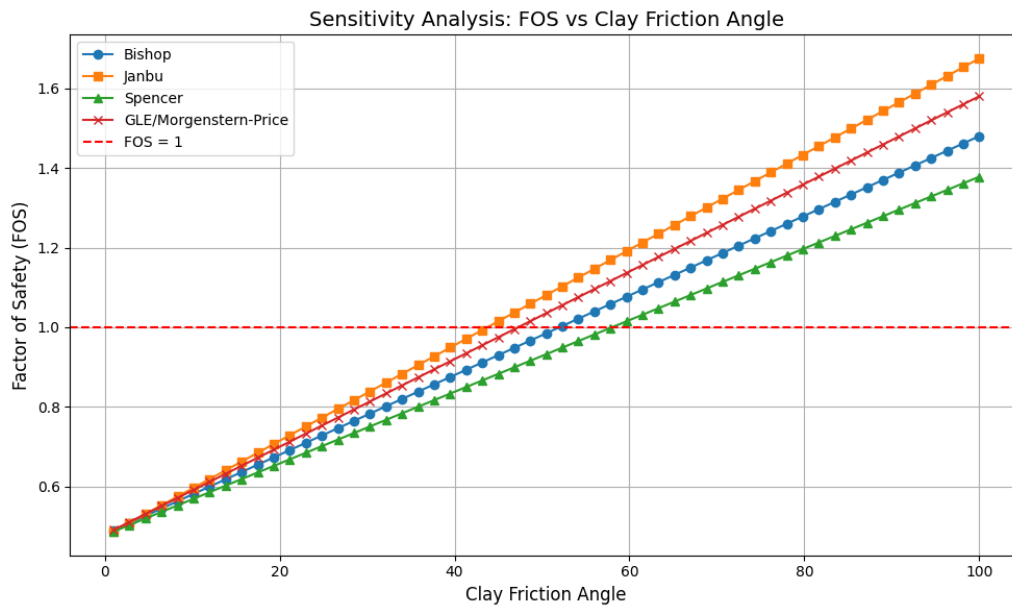
244 From a practical standpoint, the results highlight the dominant influence of the internal friction
 245 angle on slope performance. Even modest increases in ϕ produce noticeable improvements in
 246 FoS, while low ϕ values quickly lead to unsafe conditions. This emphasizes the need for
 247 accurate laboratory and field determination of friction angle in clayey soils, as uncertainty in
 248 this parameter can substantially affect design reliability and safety assessments (Khan and
 249 Wang, 2021, Phoon and Tang, 2019).



250

251

(a)



252

253

(b)

254 **Figure 6:** Sensitivity analysis of slope for (a) Clay cohesion Vs FoS (b) Friction Angle Vs

255

FoS for Ramche slope

256 The Figure 7 presents a sensitivity spider plot illustrating the impact of percentage changes in

257 cohesion and internal friction angle on the FoS, evaluated using four limit equilibrium methods:

258 Bishop, Janbu, Spencer, and Morgenstern–Price (GLE/MP). The horizontal axis represents

259 percentage variation from baseline soil parameters (–80% to +80%), while the vertical axis

260 shows the corresponding FoS values. A red horizontal line marks the failure threshold at FoS

261 = 1.0.

262 The results indicate that FoS is highly sensitive to variations in the internal friction angle across

263 all methods. As ϕ increases, FoS rises nonlinearly and significantly, crossing the failure264 threshold at approximately +35% to +40% variation. Conversely, reductions in ϕ cause a sharp

265 decline in FoS, indicating critical instability. In contrast, cohesion (c) shows minimal influence

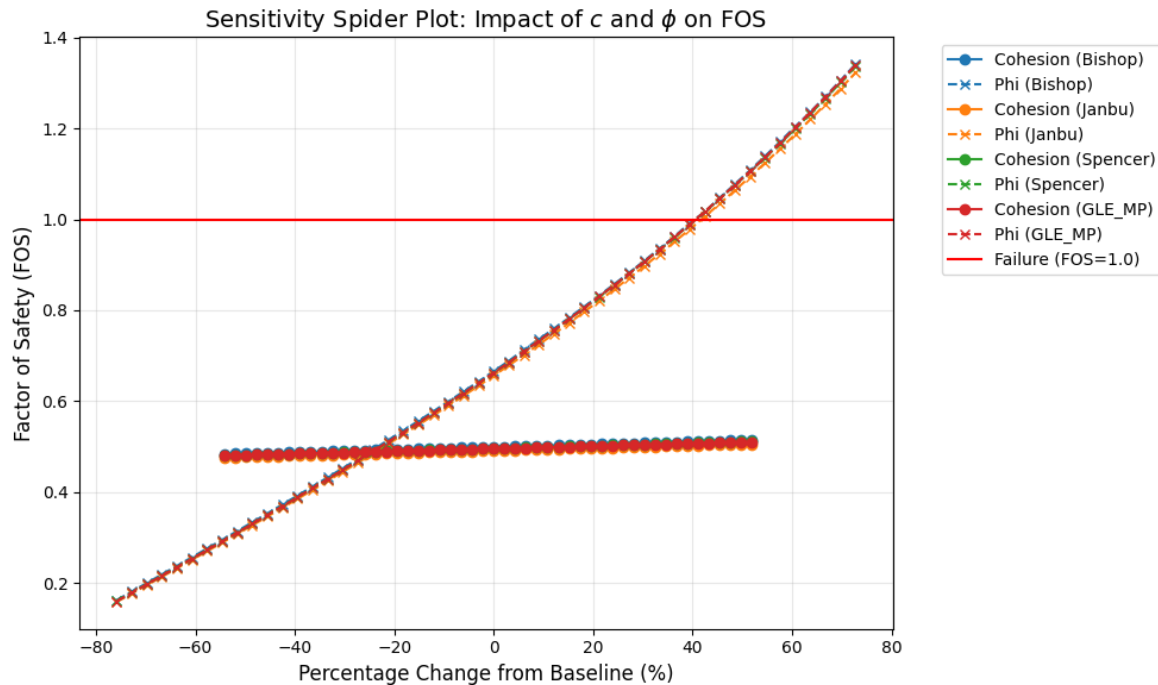
266 on FoS within the same variation range. The cohesion curves remain nearly horizontal, with

267 only slight increases in FoS as c increases, demonstrating a comparatively weak sensitivity

268 response. This consistent pattern across Bishop, Janbu, Spencer, and Morgenstern–Price

269 methods confirms that frictional resistance governs slope stability behavior in the analyzed

270 model.

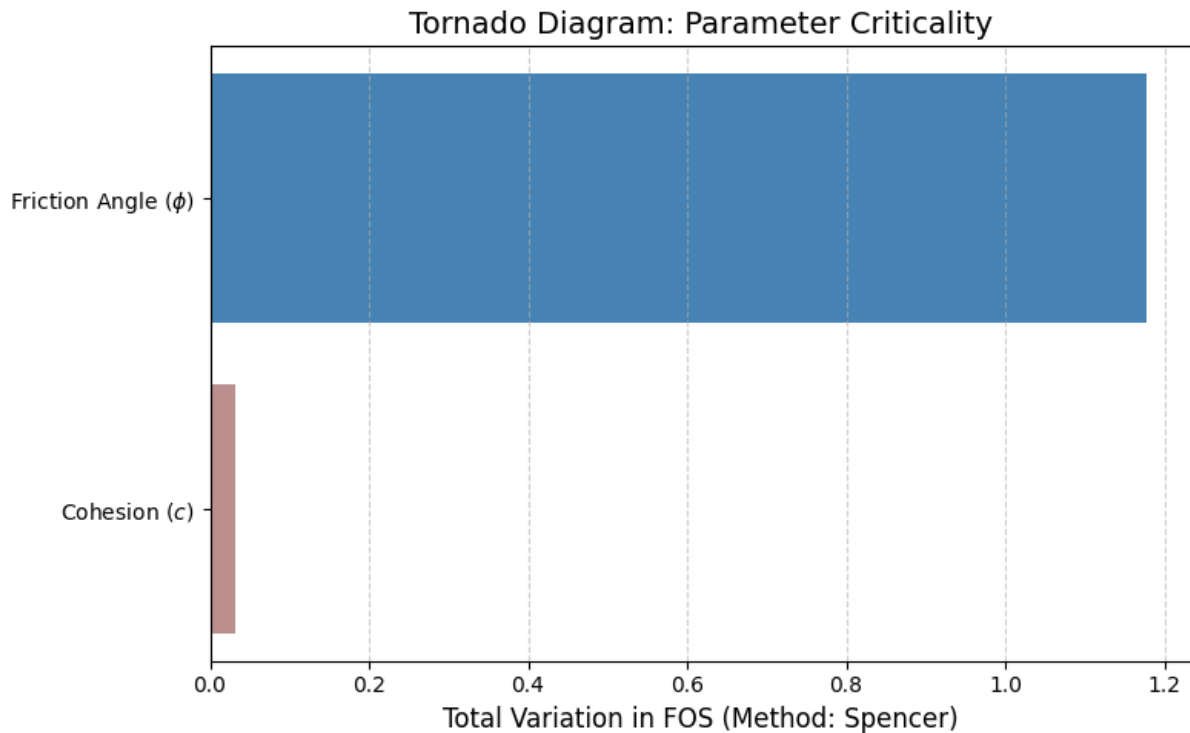


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272 **Figure 7:** Sensitivity analysis of slope and Comparison of the influence of friction angle and
 273 cohesion, on slope stability across Ramche slope (Spider plot)

274 The relative influence of shear strength parameters cohesion (c) and internal friction angle (ϕ),
 275 on the FoS was also evaluated using a Tornado diagram based on the Spencer Method as shown
 276 in Figure 8. The results indicate that ϕ is the most sensitive parameter, producing a total FoS
 277 variation of approximately 1.177, compared to 0.032 for cohesion. This confirms that slope
 278 stability is more susceptible to uncertainties in the friction angle, suggesting that the frictional
 279 component contributes more significantly to shear resistance for the studied configuration
 280 (Deng et al., 2017).

281 Also cohesion shows very low influence, its relative impact is very lower than that of ϕ (Deng
 282 et al., 2017). The sensitivity ranking ($\phi \gg c$) highlights the importance of accurate
 283 determination of ϕ through laboratory testing such as triaxial or direct shear tests. Given that
 284 both parameters generate FoS variations, the slope may be classified as highly sensitive to shear
 285 strength fluctuations. Consequently, environmental factors that reduce shear strength such as
 286 elevated pore water pressure or weathering may significantly decrease stability.



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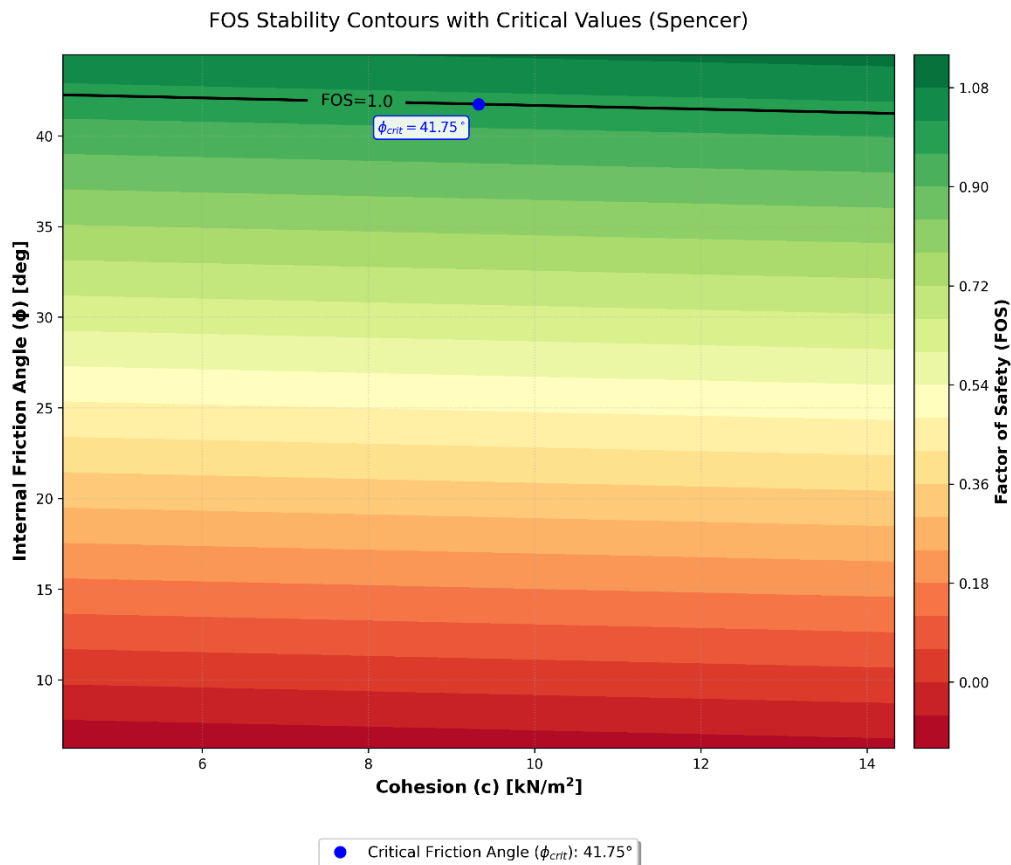
288 **Figure 8:** Sensitivity analysis of the Ramche slope to evaluate and compare the effects of
 289 cohesion and internal friction angle on overall slope stability

290 The Figure 9 presents FoS stability contours obtained using limit equilibrium method,
 291 illustrating the combined influence of cohesion (c) and internal friction angle (ϕ) on slope
 292 stability. Cohesion varies along the horizontal axis (approximately 5–14 kN/m²), while the
 293 internal friction angle ranges from about 7° to 43° on the vertical axis. The color gradient
 294 transitions from red (low FoS, unstable) to green (high FoS, stable), with a distinct contour
 295 marking FoS = 1.0, which represents the critical boundary between stable and unstable
 296 conditions.

297 The contour pattern shows that FoS is significantly more sensitive to changes in the internal
 298 friction angle than to cohesion. The predominantly horizontal contour bands indicate that small
 299 increases in ϕ produce substantial improvements in stability, whereas similar proportional
 300 changes in cohesion result in comparatively minor changes in FoS. The FoS = 1.0 line occurs
 301 at higher friction angles (around 41.75°) for low cohesion values, and slightly lower friction
 302 angles as cohesion increases, demonstrating the compensatory relationship between the two
 303 shear strength parameters.

304 The results suggest that slope stability in this analysis is primarily governed by the frictional
 305 component of shear strength rather than cohesion. Instability is concentrated in regions with
 306 low ϕ values, even when moderate cohesion is present. These findings emphasize the

307 importance of accurate determination of the internal friction angle in design and reliability
 308 assessments, as uncertainties in ϕ are likely to have a greater impact on stability predictions
 309 than comparable uncertainties in cohesion.



310

311 **Figure 9:** Sensitivity analysis of slope and Comparison of the influence of friction angle and
 312 cohesion, on slope stability across Ramche slope (FoS stability contours).

313 4. Conclusions

314 This study evaluated the sensitivity of slope stability to variations in cohesion (c) and internal
 315 friction angle (ϕ) of clay using four limit equilibrium approaches, Bishop Simplified Method,
 316 Janbu Method, Spencer Method, and Morgenstern–Price Method. The results consistently
 317 demonstrate that the internal friction angle is the dominant parameter governing the FoS for
 318 the analyzed clay slope.

319 Across all methods, FoS increased almost linearly with increasing ϕ , and reductions in ϕ led to
 320 rapid decreases in stability, frequently driving FoS below the critical threshold of 1.0. In
 321 contrast, cohesion exhibited a comparatively moderate influence. Although increases in c
 322 improved FoS, the magnitude of change was smaller than that associated with equivalent
 323 variations in ϕ . Sensitivity spider plots and stability contours further confirmed that slope

324 response is strongly controlled by the frictional component of shear strength, while cohesion
325 plays a secondary but still meaningful role.

326 The tornado diagram analysis quantified this hierarchy, showing a greater total FoS variation
327 attributable to ϕ than to c . This indicates that uncertainties in friction angle have a more
328 pronounced impact on predicted stability than comparable uncertainties in cohesion.
329 Importantly, the similarity of trends obtained from all four limit equilibrium methods suggests
330 that the sensitivity ranking ($\phi > c$) is methodologically robust, even though slight differences
331 exist in absolute FoS values.

332 From an engineering perspective, these findings underscore the critical importance of
333 accurately determining the internal friction angle in clayey soils. Given the high sensitivity of
334 FoS to ϕ , even modest errors in its estimation may significantly alter design outcomes and
335 safety margins. While cohesion should not be neglected particularly under short-term or
336 undrained conditions the frictional component ultimately governs long-term stability behavior
337 for the slope configuration analyzed.

338 Overall, the study confirms that reliable slope design and risk assessment in clay soils require
339 careful characterization of shear strength parameters, with particular emphasis on minimizing
340 uncertainty in the internal friction angle to ensure dependable and safe stability predictions.

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