TECHNIQUE FOR MEASURING MAGNITUDES AND PHASES OF VOLTAGE AND CURRENT IN BAND-SELECTIVE PARALLEL LCR CIRCUIT

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ABSTRACT

The current in the parallel LCR (inductor, capacitor and resistor) circuit depends not only on the magnitude of the applied electromotive force (emf) but also on its frequency. The circuit current in the parallel LCR circuit becomes very small in the resonating region, but at the same time, the potential difference across the LC tank becomes very large. These results are justified if there is a large induced current in the LC tank in such a way that the inductive and capacitive branch currents are nearly out of phase so that the vector sum of the currents be minimal. This theory can be verified by inserting a small series resistor in each branch. Finally, calculated magnitudes and phases of the potential differences across the newly connected resistors which are directly related to the magnitudes and phases of corresponding branch currents verify the theory.

Keywords: LCR circuit, Internal tank current, Phase difference, Antiresonance, Sensitivity

INTRODUCTION

An inductor, capacitor and resistor (LCR) circuit are essential for studying resonance phenomena. The resonating LCR circuits have a wide range of applications in designing various electronic devices (Amin *et al.*, 2018; Teymour *et al.*, 2014; Pan *et al.*, 2015; Choi *et al.*, 2015; Li & Xu, 2014; Li *et al.*, 2012; Buccella *et al.*, 2017). Both inductive reactance and capacitive reactance depend on the frequency of the ac source. The magnitude of the inductive reactance is directly proportional to the frequency, whereas, the extent of capacitive reactance is inversely proportional to the frequency (Ryder, 2012; Pipes & Harvill, 1971; Halliday *et al.*, 2001; Reitz *et al.*, 1998).

Besides, the inductive reactance induces 90° phase difference between the voltage and the current, but the capacitive reactance induces -90° phase difference between the voltage and the current (Ryder, 2012). As the frequency of the ac source gradually increases from a small value or decreases from a significant amount, the inductive reactance and capacitive reactance become equal in magnitude and opposite in sign at a particular frequency. At this frequency, called resonant frequency, these two reactances cancel each other in the series LCR circuit, and the circuit impedance becomes minimum, and thus, maximum source current flows in the circuit.

On the other hand, the source current becomes minimum or impedance becomes maximum at resonance condition in the parallel LCR circuit (Fig. 1). Since the inductor is in series to the capacitor within the LC tank loop, it induces a maximum internal current in the LC tank at the resonant frequency. The external ac source only supplies power to the LC tank equal to the power loss in the total resistance in the LC tank (Ryder, 2012). In the ideal condition, the LC tank resistance is zero, and there is no loss of power in the LC tank, and the induced current sustains forever without the external ac source supplying additional power to the LC tank. That is why the source current becomes the smallest at resonance condition (also called anti-resonance condition) in the parallel LCR circuit (Ryder, 2012).

This fact can be verified by measuring magnitudes and phase of currents and potential differences by inserting small resistors in both branches. While ascertaining the theory, the effect of additional resistors will be compared with the ideal values by using Excel-2010 program. This article will be useful for analyzing the results of a parallel LCR circuit experiment in Physics Master's degree course at different universities of Nepal.

MATERIALS AND METHODS

a) Calculation of admittance, impedance, currents and anti-resonance frequency when a resistor is present in the L-branch

The inductor is generally made from winding a conducting wire. Because of finite resistivity of the wire material, small cross-sectional area and long length, the inductor has some resistance. The effect of the coil resistance comes in series to the inductance of the coil in the equivalent circuit (Ryder, 2012). A parallel LCR circuit with a resistor in the L-branch and a sinusoidal voltage V_s sets up a sinusoidal current I in the circuit, as shown in Fig. 1. The source current I₁ is divided into I_L and I_C in the tank. The inductive (I_L) and the capacitive (I_C) currents can be expressed in terms of LC tank voltage V₀ and corresponding admittances as, I_L = Y_L V₀ and I_C = Y_C V₀.

The technique for measuring magnitudes and phases of voltage and current...



Fig. 1. Parallel LCR circuit (Ryder, 2012)

By neglecting the impedance of the current meter, the admittance of the tank circuit can be calculated as given in equation (1) (Ryder, 2012; Pipes & Harvill, 1971; Halliday *et al.*, 2001; Reitz *et al.*, 1998).

$$Y_{0} = Y_{L} + Y_{C} = \frac{1}{R_{L} + j\omega L} + j\omega C = \frac{R_{L}}{R_{L}^{2} + \omega^{2}L^{2}} + j\left(\omega C - \frac{\omega L}{R_{L}^{2} + \omega^{2}L^{2}}\right)_{(1)}$$

The anti-resonance condition of the circuit is obtained when the imaginary part of the admittance is equal to zero. Therefore, the anti-resonance frequency

$$f_{ar} = \frac{\omega_{ar}}{2\pi} = \frac{1}{2\pi} \sqrt{\frac{1}{LC} - \frac{R_L^2}{L^2}}$$
(2)

The impedance of the tank circuit at the anti-resonance condition is:

$$Z_{ar} = \frac{R_L^2 + \omega_{ar}^2 L^2}{R_L} = \frac{L}{CR_L}$$
(3)

Sensitivity

Parallel LCR circuit is usually used for selecting a particular signal from a mixture. For example, tuning a radio signal means separating the right signal from a combination of many radio waves (Comer & Comer, 2003). The sensitivity of parallel LCR circuit depends not only on the impedance of the tank circuit but also on the value of the series resistance R₁. The sensitivity of parallel LCR circuit increases with an increase in the value of R₁. The sensitivity (S) of a resonating circuit can be defined as: $S = \frac{f_0}{f_2 - f_1}$ (4)

The frequencies f_0 , f_1 and f_2 are the values of frequencies corresponding to the maximum value of the LC tank voltage (V_{0max}) and lower and upper half power points where $V_0 = 0.707 V_{0max}$.

b) Calculation of admittance, currents and antiresonance frequency when resistors are present in both branches

Magnitudes of the inductive and capacitive currents can be measured by using an ac current meter. However, their relative phase is still unknown. Additional small resistors can be added in series in both branches to measure voltages with the help of an oscilloscope. Parallel LCR circuit with resistors in both branches is shown in Fig. 2.



Fig. 2. Parallel LCR circuit with resistances present in both branches (Ryder, 2012)

Although the position of anti-resonance frequency slightly changes with the inclusion of resistances in both branches, this circuit is still useful to find out relative phases of currents through the inductor and the capacitor in the parallel LCR circuit. Since the current and voltage are in phase in the resistor, the phase difference between V_2 and V_3 in the circuit shown in Fig. 2 is also the phase difference between I_L and I_C . After measuring magnitudes and relative phase of V_2 and V_3 using a dual-channel oscilloscope, one can calculate the magnitudes of currents as; $I_L = V_2/R_2$ and $I_C = V_3/R_3$. (5)

Also, the relative phase of I_L and I_C is equal to the relative phase of V_2 and V_3 .

The admittance of the tank circuit, as shown in Fig. 3 can be calculated to be

$$Y_0 = Y_L + Y_C = \frac{1}{R_L + R_2 + j\omega L} + \frac{1}{R_3 - \frac{j}{\omega C}}$$
(6)

The admittance and the LC tank voltage (V_0) can be used to calculate currents as:

$$I_L = Y_L V_0 = \frac{1}{R_L + R_2 + j\omega L} V_0 = \left[\frac{R_L + R_2}{(R_L + R_2)^2 + \omega^2 L^2} - j \frac{\omega L}{(R_L + R_2)^2 + \omega^2 L^2} \right] V_0(7)$$

and,

$$I_{C} = Y_{C}V_{0} = \frac{1}{R_{2} - \frac{j}{\omega C}}V_{0} = \left[\frac{R_{2}}{R_{2}^{2} + \frac{1}{\omega^{2}C^{2}}} + j\frac{\frac{1}{\omega C}}{R_{2}^{2} + \frac{1}{\omega^{2}C^{2}}}\right]V_{0}$$
(8)

as well as

$$I_{1} = Y_{0}V_{0} = \left[\left\{ \frac{R_{L} + R_{2}}{(R_{L} + R_{2})^{2} + \omega^{2}L^{2}} + \frac{R_{3}}{R_{5}^{2} + \frac{1}{\omega^{2}C^{2}}} \right\} + \frac{1}{\beta} \left\{ \frac{1}{\omega^{2}C} - \frac{\omega L}{(R_{L} + R_{2})^{2} + \omega^{2}L^{2}} \right\} \right] V_{0}$$
(9)

Hari Prasad Lamichhane

Finally, the source voltage can be expressed in terms of tank voltage as

$$V_0 = \frac{V_S}{1 + Y_0 R_1} \tag{10}$$

An imaginary number can be expressed in terms of magnitude (r) and phase angle (θ) as (Ryder, 2012; Pipes & Harvill, 1971; Halliday *et al.*, 2001)

$$z = x + jy = re^{j\theta} \tag{11}$$

Where,

and $A = tan^{-1} \left(\frac{x}{-1}\right)$

Anti-resonance frequency of parallel LCR circuit with resistances present in both branches can be calculated to be (Ryder, 2012)

$$f_{ar} = \frac{1}{2\pi} \sqrt{\frac{1}{LC} \left(\frac{L - R_0^2 C}{L - R_3^2 C} \right)}$$
(13)

Where, $\mathbf{R}_0 = \mathbf{R}_{\mathrm{L}} + \mathbf{R}_2$.

The circuit shown in Fig. 2 reduces to the circuit shown in Fig. 1 when resistors R_2 and R_3 become zero. If the values of R_2 and R_3 are minimal compared to the magnitudes of inductive and capacitive reactance, the phase difference between V_2 and V_3 can approximately be taken as the phase difference between the currents flowing through the inductive and the capacitive branches in the absence of R_2 and R_3 . Excel-10 program was used to compute current and voltage and to plot their graphs. Power point is used to construct circuit diagrams and figures.

RESULTS AND DISCUSSION

One can theoretically extract some important results related to the current and voltage of the parallel LCR circuit by selecting component values. The component values were chosen as: a variable frequency sinusoidal source voltage (V_S) = 5 V peak; Inductor, L = 50 mH, coil resistance (R_L) = 100 Ω ; Capacitor, C = 0.01 μ F and resistors R_1 = 5 k Ω , R_2 = 50 Ω and R_3 = 50 Ω . The experimental circuit is shown in Fig. 3.



Fig. 3. An example of the experimental circuit for measuring relative phases of inductor and capacitor currents

a) Calculation of potential difference across the LC tank (V_0)

A graph of the calculated values of the potential difference across the LC tank (output voltage) by varying the signal frequency and keeping input voltage constant is plotted in Fig. 4. Whenever the series resistance R_1 is zero, the output voltage is always equal to the source voltage. Thus, a parallel LCR circuit with zero series resistance will be indifferent to all frequencies, and hence its sensitivity should be equal to zero. On the other hand, the output voltage monotonically increases from zero to a maximum value 4.55 V as the frequency increases from zero to 7188 Hz for the input voltage 5 V and then gradually decreases when the frequency further increases in the presence of 5 k Ω series resistance R_1 . This output voltage plot has a half-power frequency width of 3502 Hz.



Fig. 4. Dependence of the magnitude of the output potential difference (V_0) across the LC tank circuit shown in Fig. 2 with $V_S = 5 V$, L = 50 mH, C = 0.01 μ F, R_L = 100 Ω on the frequency of the applied sinusoidal voltage for a) R₁ = 0 Ω , b) R₁ = 5 k Ω , R₂ = R₃ = 0 Ω and c) R₁ = 5 k Ω , R₂ = R₃ = 50 Ω

As a measure of the sharpness of resonance, the calculated sensitivity (equation 4) of the circuit without additional resistors R_2 and R_3 was found to be 2.05. As observed in Fig. 4, the height of the output voltage and frequency width at half power frequency also depended on the additional resistors R_2 and R_3 (Fig. 2). By the inclusion of 50 Ω resistors R_2 and R_3 , the height, position and frequency width of the output voltage plot for an input 5 V signal respectively became 4.17 V, 7186 Hz, and 3788 Hz. Hence, the sensitivity of the circuit slightly decreased to 1.90 upon inclusion R_2 and R_3 . Surprisingly, at the maximum output voltage position, the V_0 was somewhat lagging in phase with the V_S when R_1 was different from zero.

Relative magnitudes and phases of voltages across the source (V_S) and the LC tank (V_0) in the circuit is shown in Fig. 3 at the frequencies a) 7103 Hz, b) 3552 Hz and c) 14206 Hz are graphically shown in Fig. 5 and the corresponding values are given in Table 1. The potential difference across the LC tank (V_0) is almost equal in

The technique for measuring magnitudes and phases of voltage and current...

magnitude to the source voltage, V_s at 7103 Hz, the resonant frequency. V_0 and V_s are in phase at the resonant frequency (Fig. 5a). At 3552 Hz, half of the resonant frequency, the output voltage reduces to slightly less than the one-third value of output voltage at the resonance frequency (Fig. 5b). The output voltage also leads the source voltage by 65.1°, thus reflecting the inductive nature of the output tank at a lower frequency. On the other hand, at 14206 Hz, the output voltage was slightly greater than one-third of the output voltage was lagging in phase with the source voltage by 69.7°. This result clearly indicates the capacitive nature of output voltage at a higher frequency.



Fig. 5. Relative magnitudes and phases of voltages across the source (V_S) and LC tank (V_0) in the typical experimental circuit shown in Fig. 3 at the frequencies (a) 7103 Hz, (b) 3552 Hz & (c) 14206 Hz

Tabl	e 1.	Ca	lcula	ted	val	ues	of	LC	tank tank	ζ.	voltage	(\mathbf{V}_0)	and
	rela	ative	e pha	ise (φ) ł	betv	vee	n V	f_0 and		V _s at th	ree s	et of
	free	quei	icies	in t	he c	ircu	uit :	sho	wn in	F	Fig. 3		

Frequency	LC tank voltage, V_0	Phase angle (ϕ) between V ₀ & V _S
7103 Hz	4.17 V	0.0°
3552 Hz	1.26 V	65.1°
14206 Hz	1.41 V	-69.7°

b) Calculated values of source current (I₁), inductor current (I_L) and capacitor current (I_C)

Computed values of source current (I_1) , inductor current (I_L) and capacitor current (I_C) as a function of frequency using experimental circuit (Fig. 3) are shown in Fig. 6. The maxima/minima values of the currents are tabulated in Table 2.



Fig. 6. Computed graph between currents and frequency with $V_s = 5 V$, L = 50 mH, $C = 0.01 \mu\text{F}$, $R_1 = 5 \text{ k}\Omega$ and $R_L = 100 \Omega$ using circuit shown in Fig. 2 when (a) $R_2 = R_3 = 0 \Omega$ and (b) $R_2 = R_3 = 50 \Omega$

As can be seen that even with the addition of $R_2 = R_3 = 50$ Ω in the circuit, the nature of the dependence of capacitor and inductor currents on the frequency does not alter. Magnitudes of capacitor and inductor currents slightly decreased, whereas the source current slightly increased. Maxima position of the capacitor current increased by 87 Hz and maxima position of the inductor current decreased by 78 Hz with the addition of 50 Ω resistors in both branches. The minimum position of the source current is also decreased by 8 Hz. The source current was equal to its real value at its minima position.

c) Relative magnitudes and phase differences among $I_1,\,I_L$ and I_C

Magnitudes and phase difference between the inductor current and capacitor current in the LC tank circuit can be obtained using the circuit shown in Fig. 3. From the experimentally measured values of magnitudes and phase differences of potential differences V_2 and V_3 using an oscilloscope and equation 5 corresponding magnitudes and phases of currents can be extracted. Time dependence of currents at the resonant frequency (f_0) and also at frequencies $f_0/2$ and $2f_0$ are shown in Fig. 7 and their numerical values are summarized in Table 3.

Table 2.	Extreme	values ar	nd positions	of current	nts in tl	he circuit	t shown	in Fig	z. 4
									4

Currents	Magnitude and position of cu	rrents for $R_2 = R_3 = 0 \Omega$	Magnitude and position of currents for $R_2=R_3=50 \ \Omega$			
	Magnitude	Frequency	Magnitude	Frequency		
I _C	2.119 mA	7656 Hz	1.952 mA	7743 Hz		
I_L	2.075 mA	6749 Hz	1.911 mA	6671 Hz		
I_1	0.091 mA	7111 Hz	0.166 mA	7103 Hz		
I ₁ Real	0.091 mA	7111 Hz	0.166 mA	7103 Hz		

Table 3. Calculated amplitudes of I_C , I_L and I_1 currents and their relative phases (ϕ) with respect to V_0 at three sets of frequency using the circuit shown in Fig. 3

Frequency	I_1 (mA)	$I_{C}(mA)$	$I_L(mA)$	ϕ_{C}	ϕ_{L}	ϕ_C - ϕ_L	ϕ_{I1}
7103 Hz	0.17	1.86	1.86	88.7°	-86.2°	174.9°	-0.1°*
3552 Hz	0.91	0.31	1.22	89.4°	-82.3°	171.7°	-79.6°
14206 Hz	0.94	1.25	0.32	87.4°	-88.1°	175.5°	85.9°

*zero phase difference position lies in the frequencies between 7103 Hz and 7104 Hz







Figure 7 and Table 3 show that inductor current was almost 180° out of phase to the capacitor current. The inductor and capacitor currents in the circuit 3 were equal in magnitudes at 7103 Hz, the resonant frequency. The source current was much smaller than either current at this frequency and was in phase with the output voltage. The source current leads the inductor current and lag capacitor current by nearly 90° each. However, at the half of the

resonant frequency, the capacitor current becomes smaller, and the inductor current dominates the source current. On the other hand, the source current was governed by the capacitor current at double of the resonant frequency.

CONCLUSION

The magnitude and phase relationships of the inductor and capacitor currents in the band selective LCR parallel circuit can be measured by inserting small resistors in both branches. Although the presence of extra small resistors in the inductive and the capacitive branches somewhat alters the magnitudes of the currents, the nature of currents does not change much.

The output voltage across the LC tank circuit becomes maximum and comes in phase with the source voltage at the resonance. The output voltage leads/lags the source voltage at lower/higher frequencies. The inductor current is almost 180° out of phase with the capacitor current in the LC tank circuit. This result suggests that the most of inductor and capacitor currents are circulating in the LC tank. As the source current is the vector sum of inductor and capacitor currents, the source current becomes smallest at the resonance because the inductor and capacitor currents are almost equal and 180° out of phase, thus, resulting in maximum circulating current in the LC tank circuit.

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